

APPLICATION NOTE 4438

# Protect Current-Sense Amplifiers Against Overvoltage Transients

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*Abstract: This application note describes methods of protecting lower-voltage current sense amplifiers from high-voltage spikes and transients. Such conditions are frequently encountered in automotive car battery operation, and are referred to as load-dump conditions.*

A similar article appeared in the October 25, 2007 issue of [Electronic Design](#).

Some current-sense amplifiers encounter overvoltages frequently. A current-sense amplifier that monitors battery-discharge currents in an automobile, for example, must withstand the high-voltage load-dump pulses produced when loads are disconnected from the battery, causing inductive spikes and overvoltages to appear at the output of the alternator. If these pulses exceed the amplifier's common-mode voltage, then one must provide external circuitry to protect the amplifier.

**Figure 1** shows an example of a protection circuit, which is composed of zener diodes Z1 and Z2, resistors R1 and R2, and diode D1. The common-mode voltage range of the MAX4372 amplifier is 0 to 28V, which is more than sufficient for measuring automotive battery voltages that vary from 6V to 18V. Load-dump voltages, however, can reach 35V and persist for 0.5 seconds, which is well over the amplifier's 30V absolute maximum rating for input voltage. The amplifier must therefore be well-protected externally.

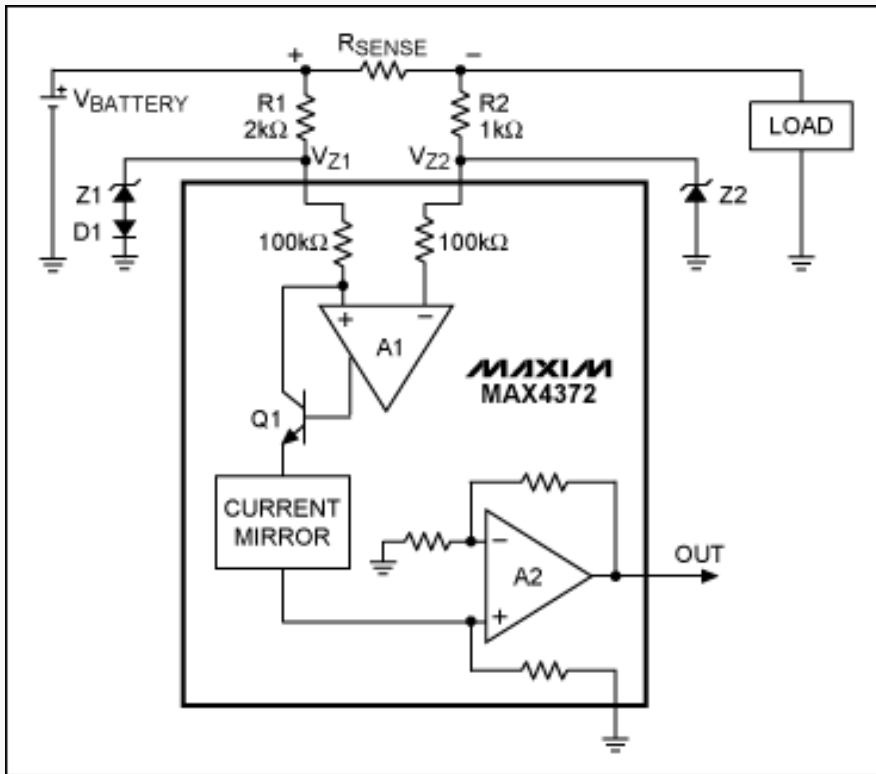


Figure 1. This current-sense amplifier has protection circuitry (upper circuit components) suitable for common-mode voltages above 30V.

You can avoid additional errors in the input offset voltage by using different values for the input-protection resistors R1 and R2 ( $2k\Omega$  and  $1k\Omega$ , respectively), thereby balancing the effect of the amplifier's unequal bias currents. For selection of these resistor values, refer to the application note 3888, "[Performance of Current-Sense Amplifiers with Input Series Resistors](#)."

Zener diodes Z1 and Z2 have nominal breakdown voltage of 24V, and are chosen to have sufficient power-dissipation capability to withstand the  $\sim 11mA$  sink currents that flow during a 35V peak load-dump condition (the 35V load-dump voltage minus a 24V clamp voltage appears across the  $1k\Omega$  series resistor R2).

**Figure 2** depicts the amplifier output in the presence of 35V load-dump pulses with D1 removed. With normal battery voltages

applied, the 1V output value is as expected (input  $V_{SENSE} = 50\text{mV}$ , and gain = 20). When a load-dump voltage appears, the zeners clamp the input common-mode voltage to about 24V, and the amplifier output makes a few transient excursions before settling down to 0V.

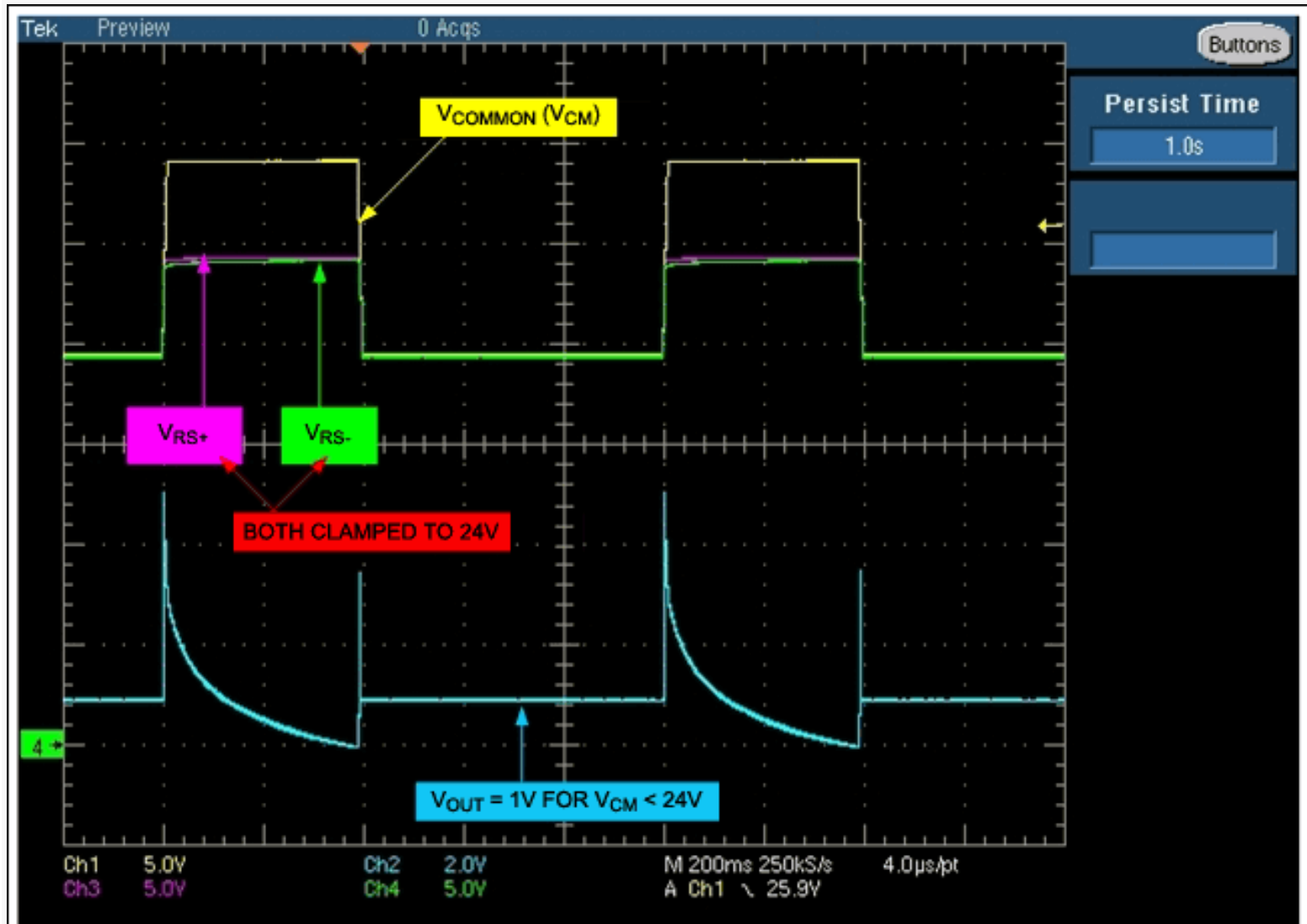
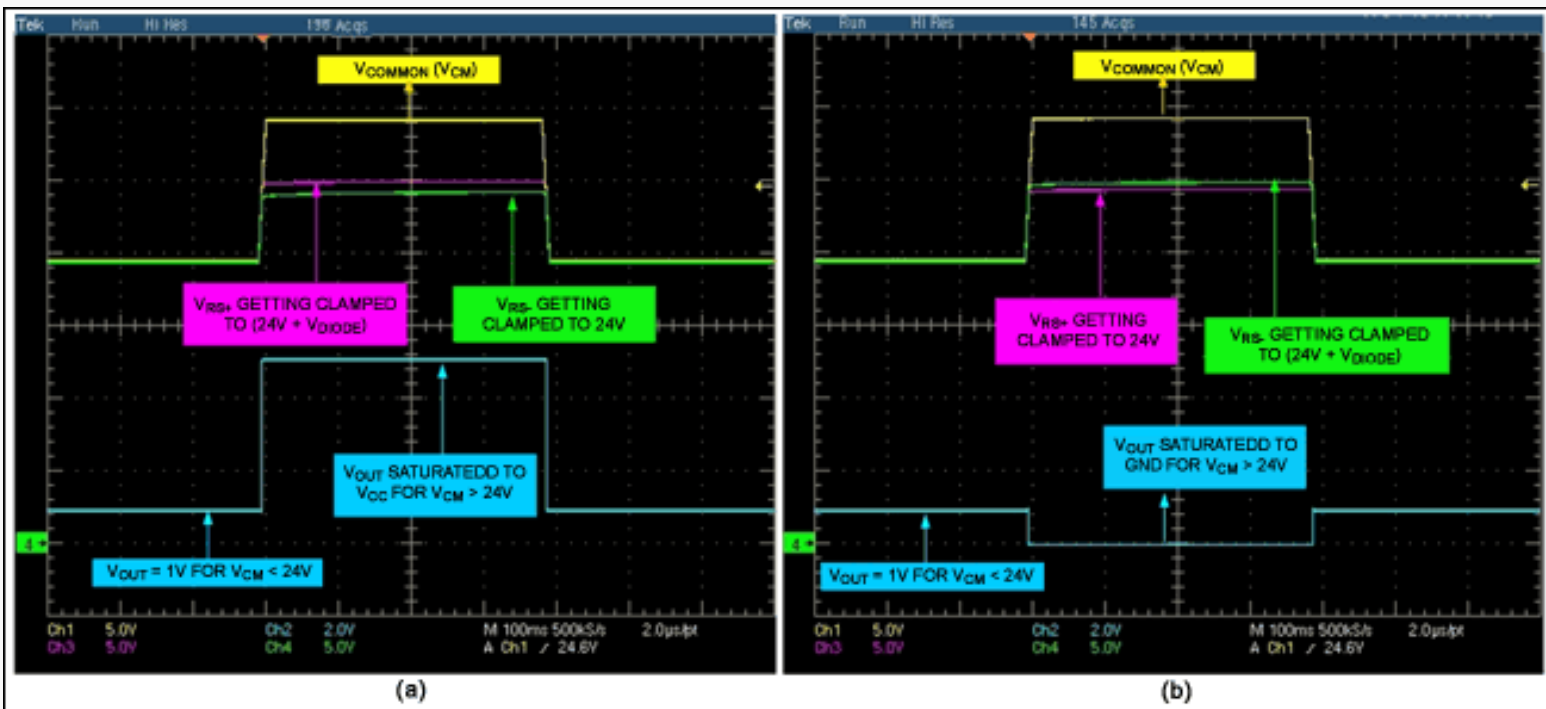


Figure 2. Operation of the Figure 1 circuit with diode D1 removed.

Though nominally 24V, the two zeners generally have slightly different breakdown voltages due to part-to-part variations and different operating currents (Z1 operates at 5.5mA and Z2 operates at 11mA). Therefore, the quantity  $(V_{Z1} - V_{Z2})$  appears as a changing differential sense voltage causing unwanted output transients. If desired, you can eliminate these transients by adding a diode in series with either Z1 or Z2. The diode forces  $(V_{Z1} - V_{Z2})$  to be either positive or negative during a load-dump condition, which in turn forces the amplifier output to one of the supply rails ( $V_{CC}$  or GND), and thereby preventing random output response during an input transient.

**Figure 3a** shows the circuit operating with the diode connected in series with Z1, which forces the amplifier output to the positive rail. **Figure 3b** shows the diode connected in series with Z2, which forces the amplifier output to the negative rail.



[More detailed image](#) (PDF, 892kB)

Figure 3. Operation of the Figure 1 circuit with D1 in series with Z1 (a), and D1 in series with Z2 (b).

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